

FUN3D v13.4 Training

Session 17:

Rotorcraft Simulations

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Session Scope

- What this will cover
 - Overview of actuator-disk models for rotorcraft
 - Overview of setup for “first principles” articulated-blade rotorcraft simulations using overset grids
 - Rigid Blades
 - Elastic Blades / Loose Coupling to Rotorcraft Comprehensive Codes
- What will not be covered
 - Rotorcraft Comprehensive Code set up and operation
 - All the many critical setup details for the “first principles” approach
- What should you already know
 - Basic time-accurate and dynamic-mesh solver operation and control
 - Rudimentary rotorcraft aeromechanics (collective, cyclic...)



Introduction

- Background
 - FUN3D can model a rotor with varying levels of fidelity/complexity
 - Actuator disk – low-fidelity representation of the rotor - when only the overall rotor influence on the configuration is needed
 - Articulated-blade system (cyclic pitch, flap, lead-lag), with or without aeroelastic effects – if detailed rotor airloads are needed
 - Rotating noninertial frame – steady-state problem for rigid, isolated, fixed-pitch blades
 - Aeroelastic effects require coupling with a rotorcraft “comprehensive” analysis (CA) code
 - CA solver can also provide rotor trim
- Compatibility
 - Coupled to CAMRAD II, DYMORE (Open Source) and RCAS CA codes
- Status
 - Less experience / testing with RCAS than with CAMRAD II / DYMORE
 - Interface provided for US Army’s HELIOS rotorcraft framework



Time-Averaged Actuator-Disk Simulations (1/3)

- Actuator disk method utilizes momentum and energy equation source terms to represent the influence of the disk
 - Original implementation by Dave O'Brien (GIT Ph.D. Thesis)
 - HI-ARMS implementation (SMEMRD) by Dave O'Brien ARMDEC adds trim and ability to use C81 airfoil tables (*Not covered*)
- Simplifies grid generation – actuator disk is automatically embedded in computational grid
- Grid refinement in the vicinity of actuator surface improves accuracy - cell sizes of “background” grid should be similar to cell sizes of actuator disk
- Any number of actuator disks can be modeled
- Requires the `--rotor` command line option for standard actuator disk
- For SMEMRD, use `hiarms_flag=.true.` in `&hiarms_actuator_disk` namelist (`fun3d.nml`) - user must request SMEMRD; not in FUN3D distribution



Time-Averaged Actuator-Disk Simulations (2/3)

- Different disk loading models available
 - **RotorType** = 1 actuator disk
 - **LoadType** = 1 constant Δp (specified thrust coefficient C_T)
 - **LoadType** = 2 linearly increasing Δp to blade tip (specified C_T)
 - **LoadType** = 3 blade element based (computed C_T)
 - **LoadType** = 4 user specified sources, not recommended
 - **LoadType** = 5 C_T and C_Q radial distributions provided in a file
 - **LoadType** = 6 Goldstein distribution with optional swirl (specified C_T and C_Q)
 - **RotorType** = 2 actuator blades (time-accurate) **Not Functional**

Time-Averaged Actuator-Disk Simulations (3/3)

- Actuator disk implementation compatible with the standard steady-state flow solver process (compressible and incompressible)
 - Standard grid formats for the volume grids
 - Standard solver input deck (`fun3d.nml`)
 - Standard output is available (`project.forces`, `project_hist.dat`, `project_tec_boundary.plt`)
 - Expect similar solution convergence as a standard steady-state case
 - Screen output includes “Rotor Force Summary” info at each iteration
- Standard actuator disk model is activated in the command line by `--rotor`
 - Rotor input deck file (`rotor.input`) is required in the local directory
 - `rotor.input` contains disk geometry and loading specifications
 - The disk geometry and loading are output in plot3d format in files `source_grid_iteration#.p3d` and `source_data_iteration#.p3d`



rotor.input File

- Constant/linear loading needs only a subset of the data in the file data (manual defines variables)

```

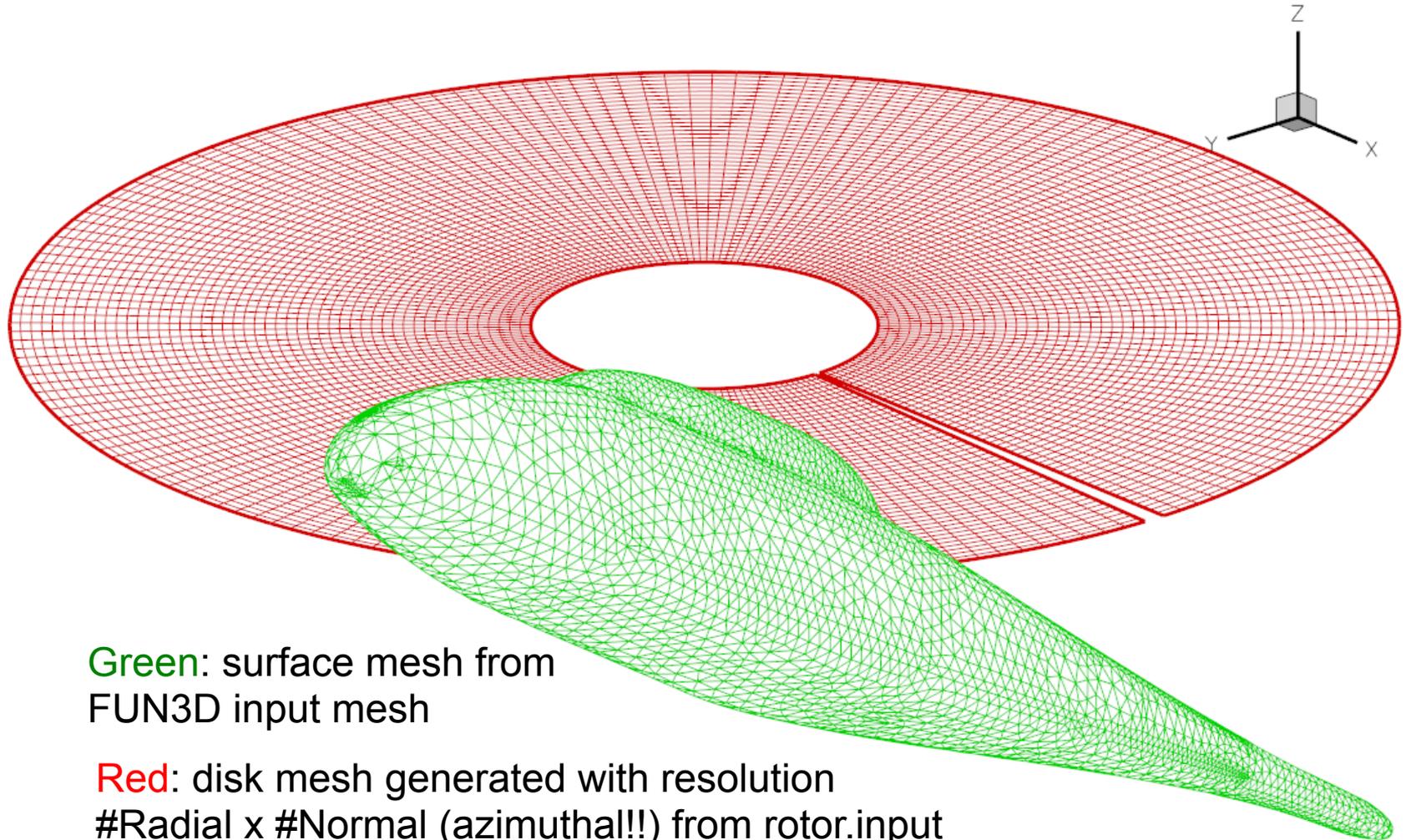
# Rotors      Uinf/Uref  Write Soln  Force Ref  Moment Ref  ! Below we set Uref = Uinf
      1      1.000      1500      0.001117   0.001297  ! Adv Ratio = Uinf/Utip
=== Main Rotor ===== ! So here Utip/Uref = 1/AR
Rotor Type   Load Type   # Radial   # Normal   Tip Weight
      1      2          50         180        0.0
X0_rotor     Y0_rotor    Z0_rotor   phi1       phi2       phi3
 0.696      0.0        0.322     0.00      -0.0      0.00
Utip/Uref    ThrustCoff  TorqueCoff psi0        PitchHing/R DirRot
 19.61      0.0064     0.00      0.0        0.0        0
# Blades     TipRadius   RootRadius BladeChord  FlapHinge/R LagHinge/R
 4          0.861      0.207     0.066     0.051     0.051
LiftSlope    alpha, L=0  cd0        cd1        cd2
 0.0        0.00      0.002     0.00      0.00
CL_max       CL_min      CD_max     CD_min     Swirl
 0.00      0.00      0.00      0.00      0
Theta0       ThetaTwist  Thetals   Theta1c    Pitch-Flap
 0.0        0.00      0.0        0.0        0.00
# FlapHar    Beta0       Betals    Beta1c
 0          0.0        0.0       0.0
Beta2s       Beta2c      Beta3s    Beta3c
 0.0        0.0        0.0       0.0
# LagHar     Delta0      Deltals   Delta1c
 0          0.0        0.0       0.0
Delta2s      Delta2c     Delta3s   Delta3c
 0.0        0.0        0.0       0.0

```

Key:
 Required for constant/linear actuator disk
 Add'l data for blade element or "first principles" simulations
 (all items must have a value, even if unused)



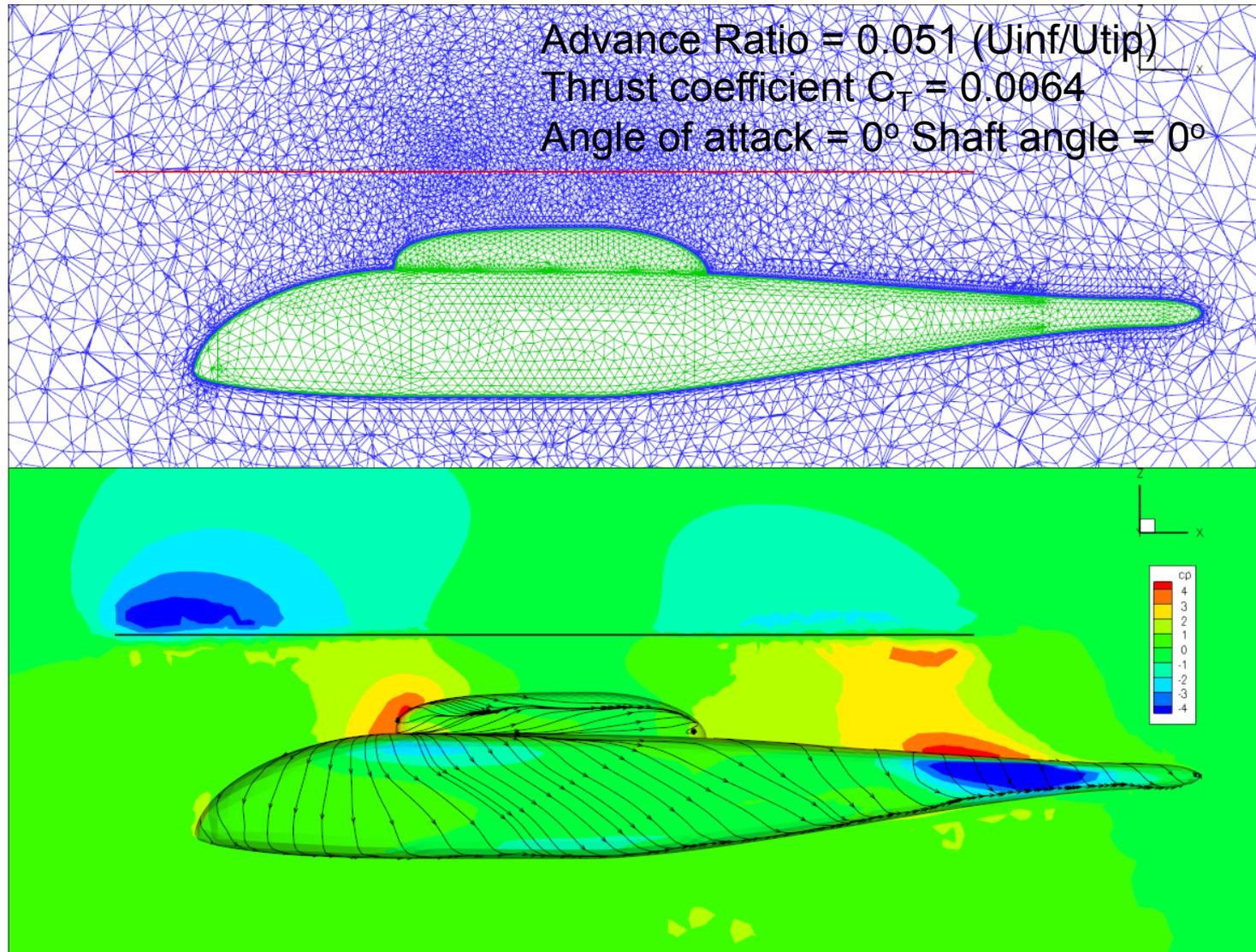
Robin Fuselage with Actuator Disk



Green: surface mesh from FUN3D input mesh

Red: disk mesh generated with resolution #Radial x #Normal (azimuthal!!) from rotor.input

Incompressible Robin/Actuator Disk



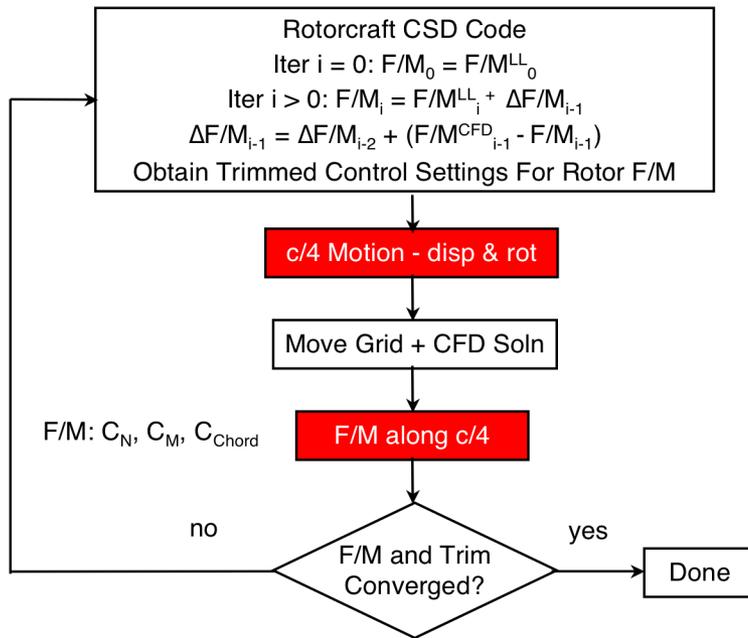
Articulated-Blade Simulations

- “First Principles” – rotor flow is computed, not modeled
 - Requires moving, overset grids; blades may be rigid or elastic
- Elastic-blade cases must be coupled to a rotorcraft CA (aka Computational Structural Dynamics, CSD) code such as CAMRAD, DYMORE or RCAS
 - The CA code provides trim solution in addition to blade deformations
 - The “interface” to CAMRAD is through standard OVERFLOW `rotor_N.onerev.txt` and `motion.txt` type files - translator codes are maintained and distributed by Dr. Doug Boyd, NASA Langley (contact d.d.boyd@nasa.gov)
 - The interface to DYMORE is similar, through `DeltaAirloads.dat`, `DymoreTotalAirloads.dat` and `Deflections.dat` type files - interface codes are maintained by Prof. Olivier Bauchau, U. Maryland
 - RCAS coupling does not require any translator codes (RCAS API)
 - FUN3D has postprocessing utility codes (utils/Rotorcraft/)
 - Many small details - we will not have time to cover

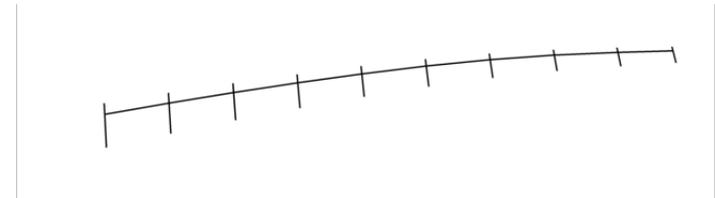


CFD/CA – Loose (Periodic) Coupling

Coupling Process



CA -> CFD



CFD -> CA

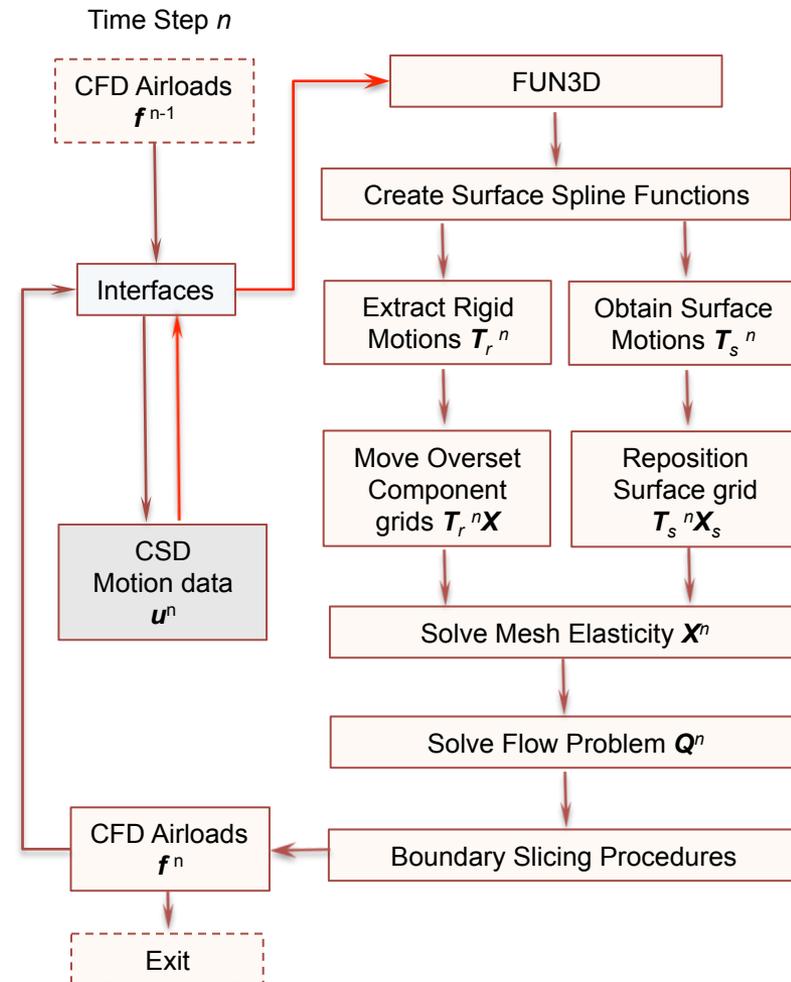


motion.txt file (blade elastic motion) and
 rotor_onerev.txt file (aero loads) common to
 FUN3D and OVERFLOW for coupling with CAMRAD

CFD/CAMRAD loose coupling implemented via
 shell script with error checking

CFD/CA – Tight Coupling

- FUN3D can also couple with CA codes in a tightly coupled manner
 - Similar to a loosely coupled procedure, but...
 - Frequent airloads-displacements data exchange between CFD and CA codes, .e.g., once per time step
 - CFD airloads applied to CA directly
 - Separated solution processes
- Support coupling with DYMORE and RCAS (less experience)
 - All data transferred in memory through interfaces - no file I/O



CFD/CSD tight-coupling algorithm

Rotor-Specific Nondimensional Input (1/2)

- Typically define the flow reference state for rotors based on the tip speed; thus in `rotor.input`, set $U_{tip}/U_{ref} = 1.0$ (data line 4)
- This way, U_{inf}/U_{ref} (data line 1) is equivalent to U_{inf}/U_{tip} , which is the Advance Ratio, and is usually specified or easily obtained
- Since the reference state corresponds to the tip, the `mach_number` in the `fun3d.nml` file should be the tip Mach number, and the `reynolds_number` should be the tip Reynolds number
- Nondimensional rotation rate: not input directly, but it is output to the screen; you might want to explicitly calculate it up front as a later check:

$$\Omega^* = U_{tip}^* / R^* \quad (\text{rad/s, } R^* \text{ the rotor radius})$$

and recall $\Omega = \Omega^* (L_{ref}^* / L_{ref}) / a_{ref}^*$ (compressible)

so with $a_{ref}^* = U_{ref}^* / M_{ref}$ and taking $L_{ref}^* = R^*$ ($L_{ref} = R$)

$$\Omega = M_{ref} (U_{tip}^* / U_{ref}^*) / R \quad (\text{compressible})$$

$$\Omega = U_{tip}^* / U_{ref}^* / R \quad (\text{incompressible})$$

Rotor-Specific Nondimensional Input (2/2)

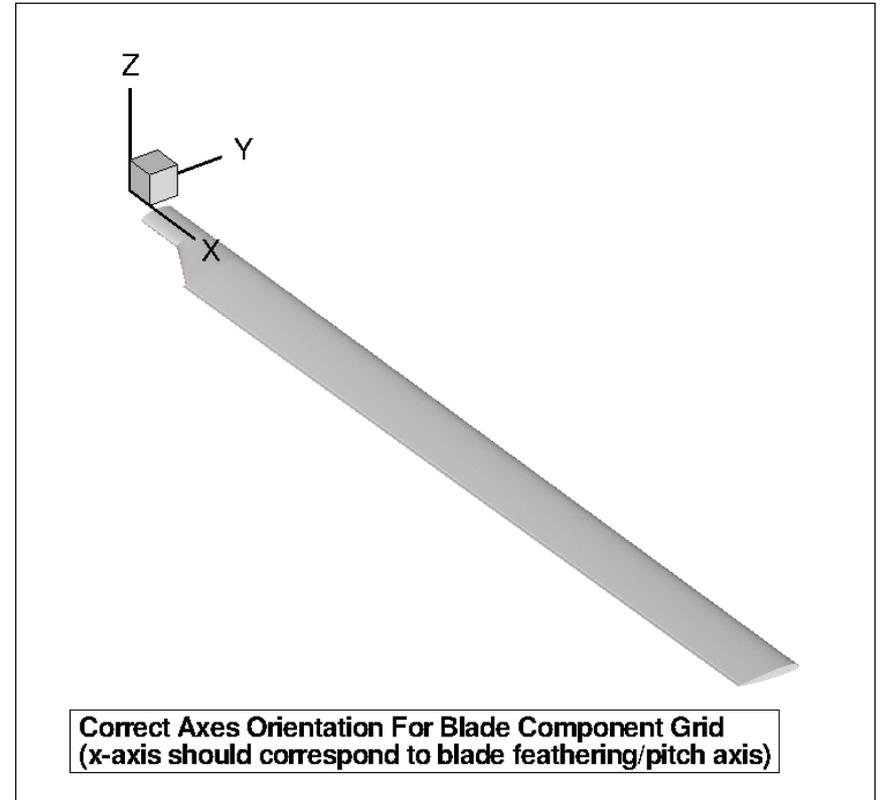
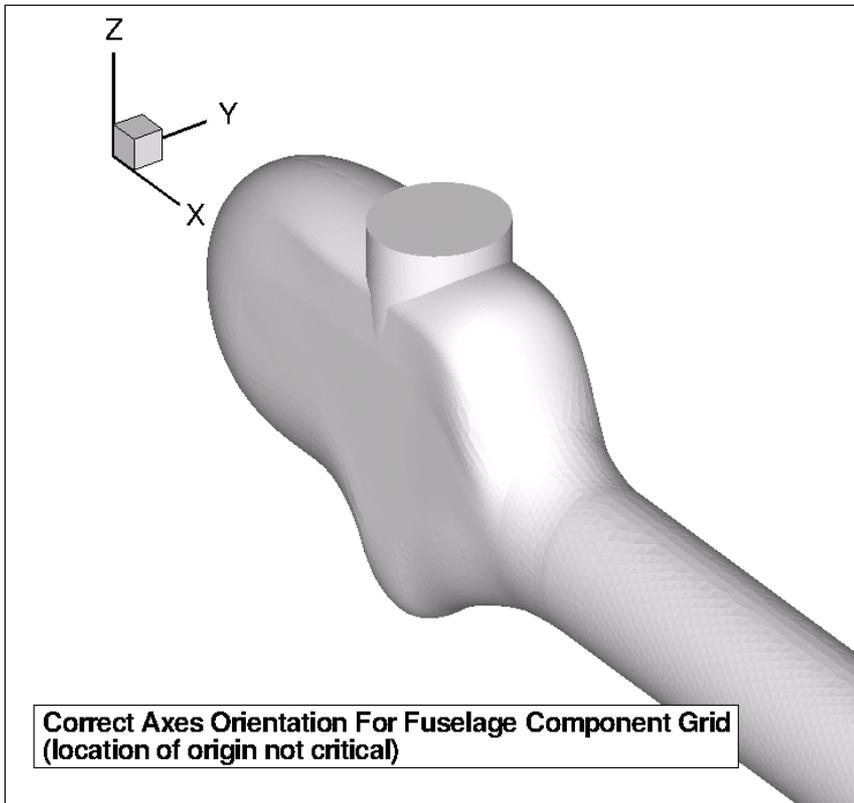
- Nondimensional time step: Note new easy Δt input introduced in slide 19
time for one rev: $T^* = 2\pi / \Omega^* = 2\pi R^* / U_{tip}^*$ (s)
and recall $t = t^* a_{ref}^* (L_{ref} / L_{ref}^*)$ (compressible)
so with $L_{ref}^* = R^*$ we have
 $T = a_{ref}^* (R / R^*) 2\pi R^* / U_{tip}^* = 2\pi R / (M_{ref} U_{tip}^* / U_{ref}^*)$ (nondim time / rev)
For N steps per rotor revolution:
 $\Delta t = 2\pi R / (N M_{ref} U_{tip}^* / U_{ref}^*)$ (compressible)
 $\Delta t = 2\pi R / (N U_{tip}^* / U_{ref}^*)$ (incompressible)
- Note: the azimuthal change per time step is output to the screen in the **Rotor info** section. Make sure this is consistent, to a high degree of precision (say at least 4 digits), with your choice of N steps per rev – you want the blade to end up very close to 360 deg. after multiple revs!
- Formulas above are general, but recall we usually have ref = tip, at least for compressible flow

dci_gen Preprocessor (1/3)

- A rudimentary code to simplify rotorcraft setup (/utils/Rotorcraft/dci_gen)
 - Uses libSUGGAR++ routines
 - Takes a single blade grid and a single fuselage / background grid (extending to far field) and assembles them into an N-bladed rotorcraft
 - Requires **rotor.input** file (number of blades defined there)
 - Creates the SUGGAR++ XML file (**Input.xml_0**) needed by FUN3D
 - Generates, using libSUGGAR++ calls, the initial (t = 0) dci file and composite grid needed by FUN3D
 - Generates the composite-grid “mapbc” files needed by FUN3D
 - Component grids *must* be oriented as shown on following slide
 - Blade must have any “as-built” twist incorporated
 - If grids do not initially meet the orientation criteria, can use SUGGAR++ to rotate them *before* using **dci_gen**

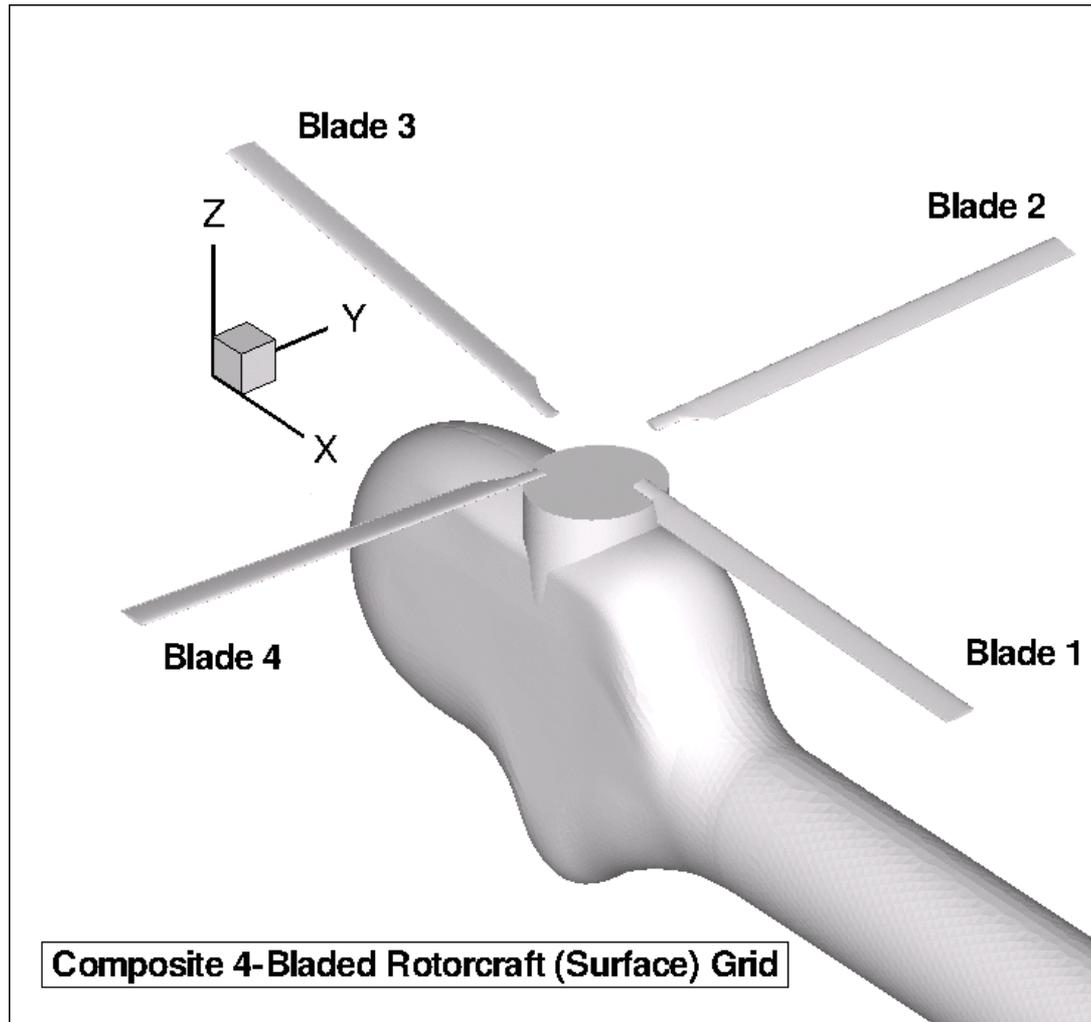
dcf_gen Preprocessor (2/3)

HART II Component Grids



dci_gen Preprocessor (3/3)

HART II *Composite* Grid



rotor.input File

- Articulated rotors need only a subset of the data (manual defines variables)

```

# Rotors      Uinf/Uref  Write Soln  Force Ref  Moment Ref  ! Below we set Uref = Utip
      1         0.245      1500        1.0        1.0        ! Adv Ratio = Uinf/Utip
==== Main Rotor =====
Rotor Type   Load Type   # Radial   # Normal   Tip Weight
      1         1           50         180        0.0
X0_rotor     Y0_rotor    Z0_rotor   phi1       phi2       phi3
      0.0        0.0         0.0        0.00       0.0        0.00
Utip/Uref    ThrustCoff  TorqueCoff psi0        PitchHinge DirRot
      1.0        0.0064      0.00       0.0        0.0466     0
# Blades     TipRadius   RootRadius BladeChord  FlapHinge  LagHinge
      4         26.8330     2.6666     1.741      0.0466     0.0466
LiftSlope    alpha, L=0  cd0        cd1        cd2
      6.28       0.00        0.002      0.00       0.00
CL_max       CL_min      CD_max     CD_min     Swirl
      1.50       -1.50       1.50       -1.50      0
Theta0       ThetaTwist  Thetals   Theta1c    Pitch-Flap
      0.0        0.00        0.0        0.0        0.00
# FlapHar    Beta0       Betals    Beta1c
      0         0.0         0.0        0.0
Beta2s       Beta2c      Beta3s    Beta3c
      0.0        0.0         0.0        0.0
# LagHar     Delta0      Deltals   Delta1c
      0         0.0         0.0        0.0
Delta2s      Delta2c     Delta3s   Delta3c
      0.0        0.0         0.0        0.0

```

Key:
Required for rigid and elastic
Additional for untrimmed rigid
 Unused (must have a value)



Input For Articulated-Blade Simulations (1/2)

- Except as noted, inputs pertain to both untrimmed/rigid-blades and trimmed/elastic blades
- Run as time-dependent, so will need to set time step as per slide 14
- Required additional `fun3d.nml` input

```
&global
  moving_grid = .true.
  slice_freq = 1           (optional if rigid untrimmed)
/
&rotor_data
  overset_rotor = .true.
/
&overset_data
  overset_flag      = .true.
  dci_on_the_fly    = .true.   (potentially optional if rigid)
  dci_period        = 360     (assuming 1 deg. per time step)
  reuse_existing_dci = .true.
/
&nonlinear_solver_parameters
  time_step_dpsi    = 1.0     (azimuthal deg. per time step)
/
```



Input For Articulated-Blade Simulations (2/2)

- The `moving_body.input` file is somewhat simplified since much of the motion description is handled by `rotor.input` – all we need do is to define the moving bodies and provide the SUGGAR++ XML file if required

```
&body_definitions
  n_moving_bodies      = 4                (e.g., for 4-bladed rotor)
  body_name(1)         = 'rotor1_blade1' (same as in xml file)
  n_defining_bndry(1) = 2
  defining_bndry(1,1) = 3
  defining_bndry(1,2) = 4
  mesh_movement(1)    = 'rigid+deform' (or just 'rigid' for
                                       for rigid blade case)
  ... (etc. for blades 2-4)
/
&composite_overset_mesh
  input_xml_file = "Input.xml_0" (potentially optional if rigid
                                  and have precomputed dci)
/
```

- Note: `motion_driver` *not* set in `&body_definitions` (in contrast to any other moving-grid case); also *no* `&forced_motion` input

CAMRAD Considerations

- User must set up basic CAMRAD II scripts; the `RUN_LOOSE_COUPLING` script provided with FUN3D requires 3 distinct, but related CAMRAD scripts
 - `basename_ref.scr`
 - Used to generate the reference motion data used by CAMRAD
 - Set this file to use rigid blades; zero collective/cyclic; no trim
 - `basename_0.scr`
 - Used for coupling/trim cycle “0”
 - Set up for elastic blades with trim; use CAMRAD aerodynamics exclusively (no delta airloads input); simplest aero model will suffice
 - `basename_n.scr`
 - Used for all subsequent coupling/trim cycles
 - Set up for elastic blades with trim; use same simple CAMRAD aerodynamics but now with delta airloads input

DYMORE Considerations

- For coupling with DYMORE, `fsi_tight_coupling.input` file is required - both loose and tight coupling procedures

```
./dymore5_baseline/uh60_4bl.dym      ! Main DYMORE input
1.0                                   ! grid unit ratio
1                                     ! ramping parameters for motions
```

- You can put all DYMORE input decks under the FUN3D run directory - but suggest to create a subdirectory to store all DYMORE input decks (and outputs); in the above example, `./dymore5_baseline` is the subdirectory
- Note that more info will be added to `fsi_tight_coupling.input` file for FUN3D/DYMORE multidisciplinary design optimization (referred to Multidisciplinary Design Session)

Blade Surface “Slicing”

- Boundary surface (rotor blade) slicing is *required* for coupled CFD/CA simulations; also useful for rigid-blade cases - this is what generates the data in `rotor_1.onerev.txt`, `rotor_1.onerev_inertial.txt`

```
$slice_data
  replicate_all_bodies      = .true.           ! do the following the same on all blades
  output_sectional_forces  = .false.          ! just lots of data we usually don't need
  tecplot_slice_output     = .false.          ! ditto
  slice_x(1)               = .true.,          ! x=const slice - in original blade coords
  nslices                  = -178,           ! no. slices; "-" means give start and delta
  slice_location(1)        = 2.8175,         ! x-location to slice (starting slice)
  slice_increment           = .134166666666   ! delta slice location each successive slice
  n_bndrys_to_slice(1)     = 1,              ! 1 bndry to search
  bndrys_to_slice(1,1)     = 2,              ! indicies:(slice,bdry) lumping made life easy
  slice_frame(1)           = 'rotor1_blade1', ! ref. frame in which to slice - use body name
  te_def(1)                = 20,             ! look for 2 corners in 20 aft-most segments
  le_def(1)                = 30,             ! search 30 fwd-most pts for one most distant from TE
  chord_dir(1)             = -1,             ! Recall goofy original blade coord system
```

/

- Note: “slicing” useful for applications other than rotorcraft; see website



Untrimmed Rigid-Blade Simulations

- Overview of the basic steps
 1. Prepare rotor blade and fuselage grids, with proper axis orientation
 2. Set up the **rotor.input** file based on flight conditions
 3. Run the **dci_gen** utility to create a composite mesh and initial dci data
 4. Set up **fun3d.nml** and **moving_body.input** files
 5. Optionally set up the **&slice_data** namelist in the **fun3d.nml** file
 6. Run the solver; the number of time steps required is case dependent – usually at least 3 revs for rigid blades



Trimmed, Elastic-Blade Simulations (1/2)

- Overview of the basic steps; steps 1-4 are the same as for the untrimmed rigid-blade case; use of CAMRAD is assumed
 5. Set up the `&slice_data` namelist; set `slice_freq = 1` *not optional*
 6. In `&rotor_data` namelist, set `comprehensive_rotor_coupling='camrad'`
 7. Set up the 3 CAMRAD run-script templates as per slide 21
 8. Set up the `RUN_LOOSE_COUPLING` run script (a c-shell script geared to PBS environments); user-set data is near the top – sections 1 and 2
 9. Set up the `fun3d.nml_initial` and `fun3d.nml_restart` files used by the run script; typically set the time steps in the initial file to cover 2 revs, and $2/N_{\text{blade}}$ revs in restart version
 10. Before using the run script make sure all items it needs are in place
 11. Number of coupling cycles required for trim will vary, but 8-10 is typical for low-moderate thrust levels; high thrust cases near thrust boundary may require 10-15; user judges acceptable convergence

Trimmed, Elastic-Blade Simulations (2/2)

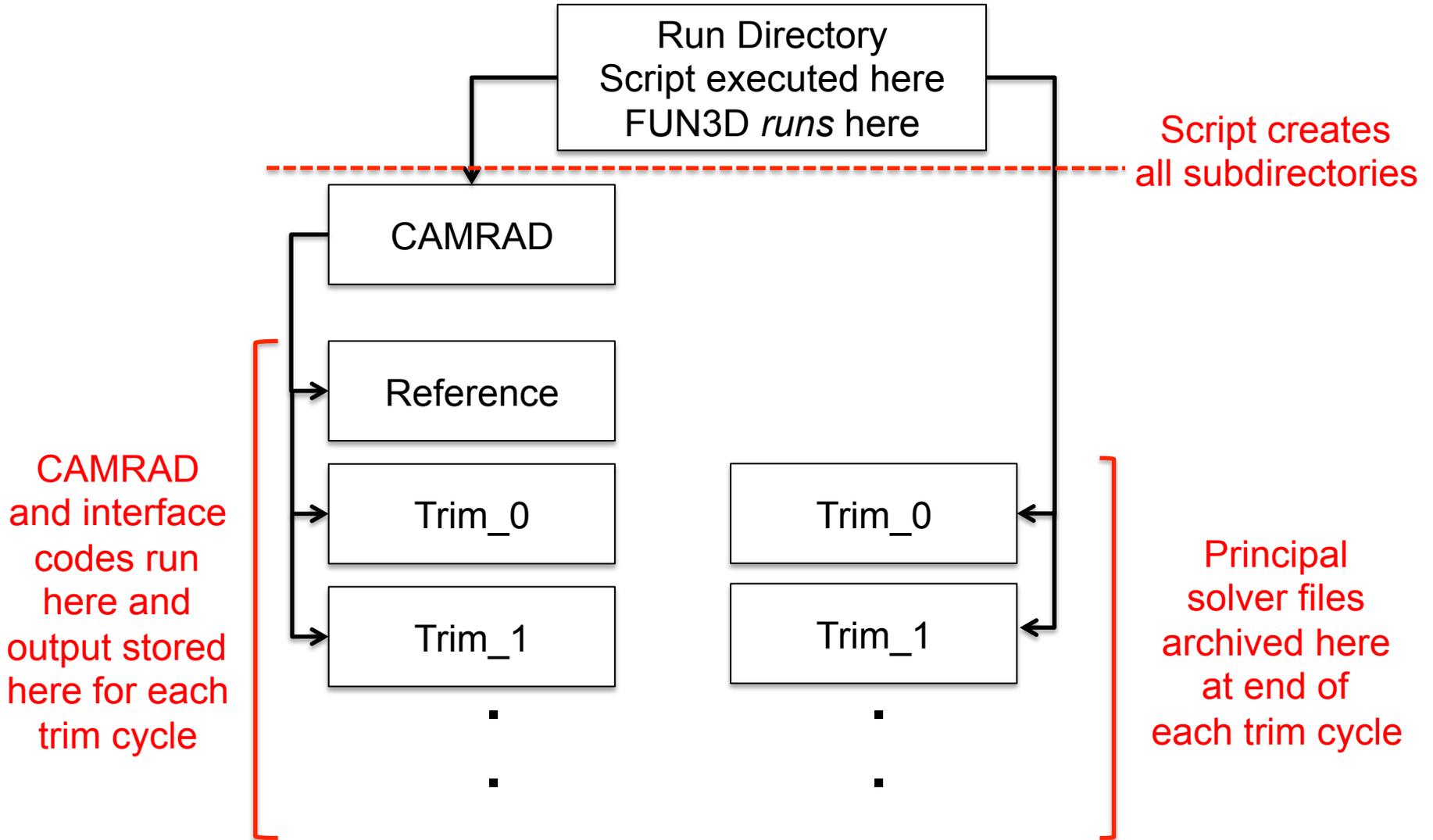
- Overview of the basic steps; steps 1-5 are the same as for CAMRAD case; use of DYMORE is assumed (*loose coupling*)
 6. Set up `&rotor_data` namelist; set

```
comprehensive_rotor_coupling = 'dymore'
```

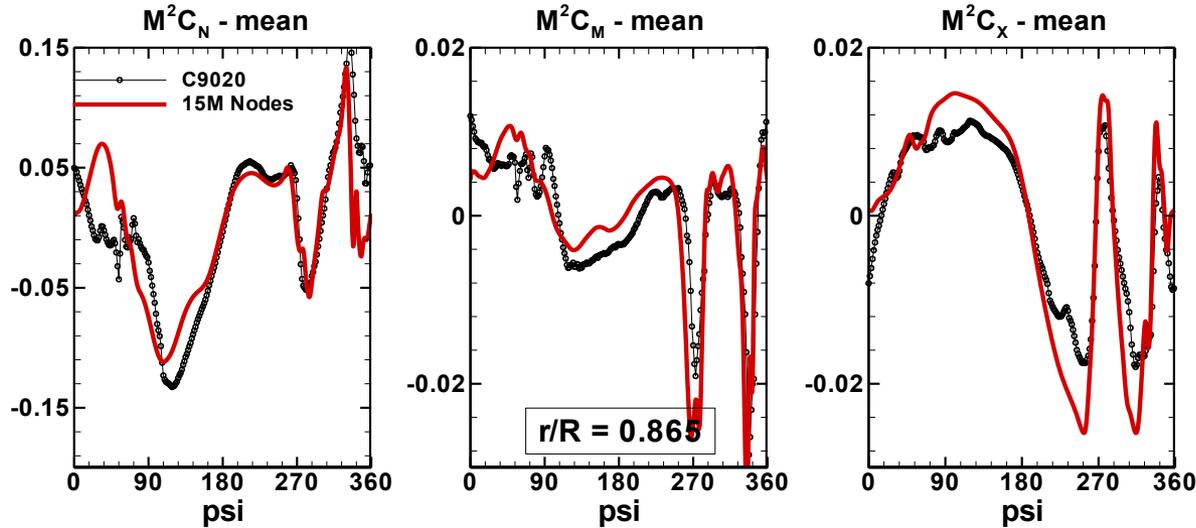
```
niters_cfd(1,1:2) = 360, 180
```

- number of CFD time steps used for 1st and all subsequent loose-coupling iterations before airloads transferred to DYMORE
 7. Set up `fsi_tight_coupling.input` file as per slide 22
 8. Run DYMORE static analysis (no wind)
 9. Run DYMORE dynamic analysis (i.e., no delta airloads; using internal low-fidelity aerodynamics) to get initial blade deflections with trim
 10. Run FUN3D - total number of CFD time steps for all coupling iterations is controlled by `steps` parameter in `&code_run_control` namelist
- FUN3D runs *tight coupling* - in `&rotor_data` namelist, set `comprehensive_rotor_coupling = 'dymore_tight'`; in `fsi_tight_coupling.input` file, set DYMORE input name accordingly

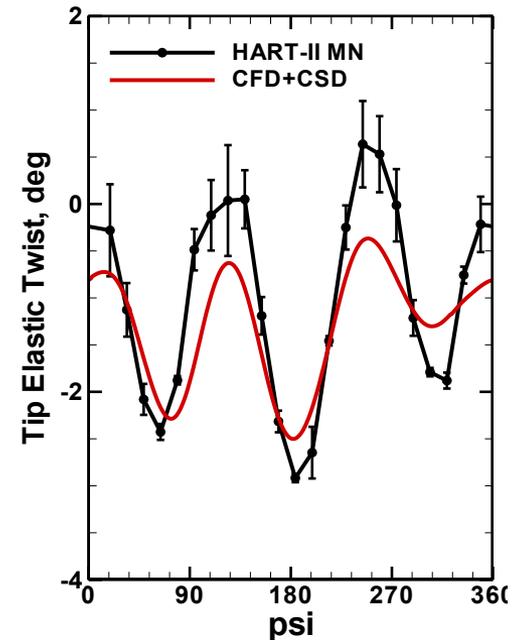
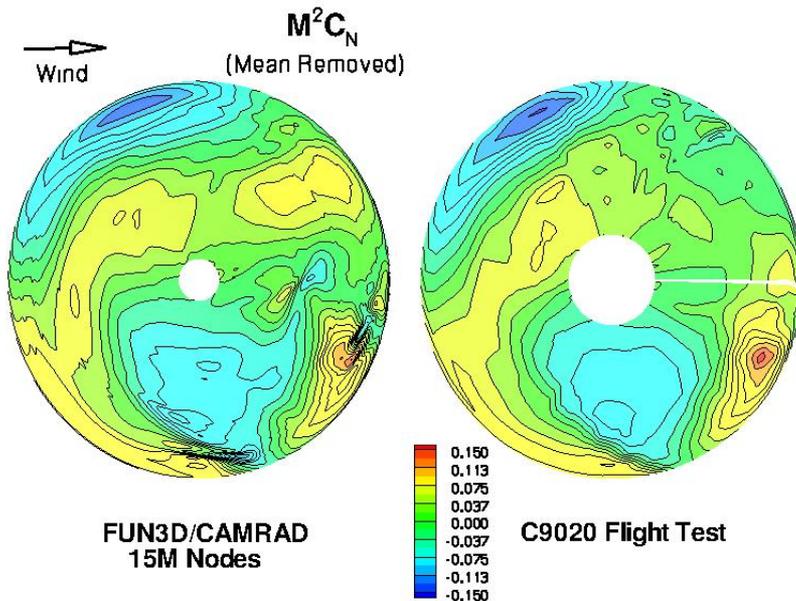
RUN_LOOSE_COUPLING Directory Tree (CAMRAD)



Postprocessing (utils/Rotorcraft/)



Sample Plots Possible Via
process_rotor_airloads.f90
Output



Noninertial Reference Frame (1/2)

- For *isolated, rigid* an improvement in solution efficiency may be obtained by transforming to a coordinate system that rotates with the rotor
- FUN3D implements a very limited subset of possible noninertial frames:
 - Constant rotation rate
 - Free-stream flow limited to
 - Quiescent (e.g., rotor in hover)
 - Flow aligned with axis of rotor (e.g., ascending/descending rotor; prop in forward flight at 0 AoA)
- In this noninertial rotating frame, the flow is assumed steady
- Can be used in conjunction with overset grids to allow pitch/collective changes to rotor without regridding
- The noninertial capability has other limited applications in addition to rotors – e.g., aircraft in a steady loop

Noninertial Reference Frame (2/2)

- `fun3d.nml` input for noninertial frame solutions (example for rotor spinning about z-axis)

```
&noninertial_reference_frame
  noninertial = .true.
  rotation_center_x = 0.0   !rotation axis passes through this pt.
  rotation_center_y = 0.0
  rotation_center_z = 0.0
  rotation_rate_x    = 0.0
  rotation_rate_y    = 0.0
  rotation_rate_z    = 0.2
```

/

- The nondimensional rotation rate is determined as shown on slide 13
- Flow-visualization output (boundary, volume, sampling) will be relative to the noninertial frame

